Mathematical Modelling of MHD Couette flow of Burger's fluid in annuli

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Abstract

This paper presents a semi-analytical study for the MHD Couette flow of Burger's fluid. The flow of an incompressible conducting Burgers fluid in the presence of a uniform transverse magnetic field between two concentric cylinders that is moved suddenly is considered. By the application of Laplace Transformation (LT) and Riemann-sum approximation method (RSM), the semi-analytical expressions for velocity and the skin friction are obtained. The influence of various dimensionless parameters emerging in the model such as time (t), magnetic parameter (M), relaxation (λ), retardation (θ) times and Burger's (β) parameter on the velocity and skin friction are presented graphically and discussed. It is found that the relaxation time helps the flow pattern, while material constants resist the fluid flow. Finally, earlier solutions to the Oldroyd-B fluid, Maxwell fluid and Newtonian fluid appears as the limiting case of the present solution.

Keywords: Burger's fluid, MHD, Couette flow, Annuli, Riemann-sum approximation, Rheometer

1. Introduction

Studies of unsteady MHD flows has gained increasing interest from the practical point of view due its application in many natural phenomena and engineering problems. This is due to the fact that fluid transient may be expected at the start up time of MHD devices such as, MHD power generators and pumps, MHD accelerators, nuclear reactors and so forth. The first study of MHD flow of non-Newtonian fluids was carried out by Sarpkaya (1961). Since then, several other investigations considering the MHD flow of non-Newtonian fluids were carried out and as such it becomes an active area of research. Ersoy (1999) examined the MHD flow between eccentric rotating disks for an Oldroyd-B fluid. Liu, et al. (2011) and Zheng et al. (2011) and (2012) analyzed the MHD flow of generalized Oldroyd-B fluid for different physical situations using fractional derivatives. Hayat et al. (2004) considered the motion of electrically conducting incompressible Oldroyd-B fluid between two infinitely extended non-conducting parallel plates under a uniform transverse magnetic field, fixed relative to the fluid. Their results showed that the flow field is appreciably influenced by the applied magnetic field, the rotation and the material parameters of the fluid. An exact solution for flows of an electrically conducting Oldroyd-B fluid over an infinite oscillatory plate in the presence of a transverse magnetic field was obtained by Hayat and Hutter (2002). Khan et al. (2012) derived exact solutions of Stokes second problem for MHD Oldroyd-B fluid. Sultan et al. (2013) presented analytical solution for the unsteady magnetohydrodynamic (MHD) flow of Oldroyd-B fluid in long porous rectangular crosssection. Recently Khan et al. (2013) presented an analytical solution to the problem of MHD flow of an Oldroyd-B fluid induced by the impulsive motion of a plate between two side walls perpendicular to the plate an extension to the work by Fetecau et al. (2011). The analytical solutions are carried out by using the Fourier sine and Laplace transforms. An exact solutions corresponding to the axial flow of an Oldroyd-B fluid in an annular region between two infinite circular cylinders are established by Jamil et al. (2012).



The nonlinearity nature of relationship between shear stress and shear rate that occur due to the variation of viscosity at a given temperature and pressure in non-Newtonian fluid makes it uneasy to have a constitutive relation that predicts their behaviors. This brought about the growing concern in the processing industries and elsewhere where materials whose flow behavior in shearing cannot be characterized by Newtonian relationship. There are many investigations that has been done on the dynamics of non-Newtonian fluids. Hence, of significance to this present study are those on Burger's fluid whose application are found in the field of Biological and Chemical analysis, drug delivery, bacteria detection, slurries and many others. Extensive applications of Burgers fluid can be found in the literature and we refer readers to the works of Burger (1935), Krishnan and Rajagopal (2004), Chen et al (2004), Ravindran et al (2004), Ravindran (2004), Chun et al. (2006), Chen et al. (2006), Khan et al. (2010), Hyder (2010), Yaqing Liu et. al. (2011), Quintanilla and Rajagopal (2012), Khan (2013), Alsaedi et al (2013), Ahmad et al (2014), Jianhong et al. (2015), Yan Zhang et. al (2017), Kashif et al. (2018), Madeeha et al. (2018), Nirmala and Kumari (2019), Fetecau and Dumitru (2021), Maria et al. (2022), and Musa et al. (2023).

Motivated by the above mentioned works, this paper presents an extension of Sani and Jha, (2022) from an Oldroyd-B fluid to the Burgers' fluid. The expressions for the velocity and shear stress are given in Laplace transform domain with the aid of modified Bessel equations which fulfill all the imposed conditions. Inversion of the Laplace transformation is done numerically by using MATLAB software. At the end, influence of various parameters like relaxation and retardation time parameters, material constants, time and viscosity parameters are graphically presented.

2. Governing Equations

The flow of an unsteady incompressible and electrically conducting Burgers' fluid filling the gap between two horizontal concentric cylinders of infinite length governed by the following equations are considered.

$$\nabla V = 0.$$

$$\rho \frac{dV}{dt} = -\nabla P + \nabla S + J \times B.$$
⁽¹⁾
⁽²⁾

The Cauchy stress tensor T and the extra stress tensor S of an incompressible Burgers' fluid defined by the constitutive equation as;

$$T = -pI + S.$$
(3)
and
$$S + \lambda \frac{Ds}{Dt} + \beta \frac{Ds}{Dt} = \mu \left(1 + \theta \frac{D}{Dt}\right) A_1.$$
(4)

Where *p* is the pressure, *I* is the identity tensor, μ , λ , θ , and β are the material constants and respectively known as the viscosity coefficient, the relaxation time, retardation times and Burger's parameter. It is assumed that $\lambda \ge \theta \ge \beta \ge 0$. A_1 is the first Rivlin–Ericksen tensor and $\frac{D}{Dt}$ is the upper convicted derivative defined by

$$A_{1} = \nabla V + (\nabla V)^{T}.$$
and
$$\frac{DS}{Dt} = \frac{\partial S}{\partial t} + (V \cdot \nabla)S - STV - (\nabla V)^{T}S.$$
(6)

Where V being the velocity vector, ∇ is the gradient operator, the superscript T denotes the transpose operation. In the present problem eq. (6) reduces to

$$\rho \frac{dV}{dt} = \nabla T + \rho b. \tag{7}$$

Where ρ is the fluid density, b is the body force field, $\frac{d}{dt}$ is the material derivative. The velocity field and the stress is defined as:

$$V = u(r, z, t)i, \quad S = s(r, z, t)i.$$
(8)

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Where \hat{i} and u are the unit vectors and velocity in the radial direction of the cylindrical coordinate system respectively.

3. Mathematical Formulation and Solution of the Problem

In this problem, we consider flow formation of an unsteady and electrically conducting incompressible Burgers' fluid due to sudden motion of outer cylinder of an annulus. The fluid flow between the two cylinders in the presence of magnetic field acting perpendicular to the flow direction, where a and b are the radii of the inner and the outer cylinders respectively. We assume that the magnetic Reynolds number is very small which correspond to negligible induced magnetic field compared to the externally applied one as discussed in Pai, (1962). At time $t' \leq 0$, the fluid and the cylinders are assumed to be at rest. However, when t' > 0 the outer cylinder begins to move in its own plane with a velocity Ut'^n , where U a constant is and the inner cylinder remains at rest. Since the cylinders are of infinite length and the flow is fully developed, all physical variables are functions of r' and t'. Furthermore, assuming that no applied and polarization voltage exists. Under these assumptions, the mathematical model governing the present physical situation is given as;

$$\left(1 + \lambda \frac{\partial}{\partial t'} + \beta \frac{\partial}{\partial t'}\right) \frac{\partial u'}{\partial t'} = \left(1 + \theta \frac{\partial}{\partial t'}\right) \left[\frac{\partial^2 u}{\partial r'^2} + \frac{1}{r'} \frac{\partial u'}{\partial r'}\right] - \frac{\sigma B_o^2}{\rho} U'.$$
⁽⁹⁾

Equation (9) is valid when the magnetic field is fixed relative to the fluid. If the magnetic field is fixed relative to the moving cylinder, Eq. (9) can be replaced with the following equation;

$$\left(1 + \lambda \frac{\partial}{\partial t'} + \beta \frac{\partial}{\partial t'}\right) \frac{\partial u'}{\partial t'} = \left(1 + \theta \frac{\partial}{\partial t'}\right) \left[\frac{\partial^2 u'}{\partial r'^2} + \frac{1}{r'} \frac{\partial u'}{\partial r'}\right] - \frac{\sigma B_o^2}{\rho} \left(U' - Ut''\right)$$
(10)

Equations (9) and (10) can be written together as follows;

$$\left(1 + \lambda \frac{\partial}{\partial t} + \beta \frac{\partial}{\partial t}\right) \frac{\partial u}{\partial t} = \left(1 + \theta \frac{\partial}{\partial t}\right) \left[\frac{\partial^2 u}{\partial r'^2} + \frac{1}{r} \frac{\partial u}{\partial r'}\right] - M^2 \left(1 + \lambda \frac{\partial}{\partial t} + \beta \frac{\partial}{\partial t}\right) (U' - Kt'')$$
(11)

where,

$$K = \begin{cases} 0 & \text{When } B_0 \text{ is fixed relative to the fluid.} \\ 1 & \text{When } B_0 \text{ is fixed relative to the moving cylinder.} \end{cases}$$

The initial and boundary conditions for the problem are

$$u' = \begin{cases} 0 & a \le r \le b & and & t' \le 0 \\ 0 & at & r' = a & t' > 0 \\ ut'^{n} & at & r' = b & t' > 0 \end{cases}$$
(12)

The mathematical model described by Eq. (11) and (12) is the general representation of the unsteady flow formation for the MHD Couette flow of a Burger's fluid between two infinite concentric cylinders when the outer cylinder is moving with Ut'^n . We set out to find solution for the impulsive movement of the outer cylinder, which corresponds to n = 0;

3.1 Solution

Employing the non-dimensional quantities

$$t = \frac{t \upsilon}{a^2}, \ r = \frac{r}{a}, \ u = \frac{u}{U}, \ \lambda = \frac{\lambda \upsilon}{a^2}, \ \theta = \frac{\theta \upsilon}{a^2}, \ \beta = \frac{\beta \upsilon}{a^2}, \ M^2 = \frac{\sigma B_0^2 a^2}{\rho \upsilon}, \ r^* = \frac{b}{a}.$$
 (13)

we have the following dimensionless governing equation;

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$$\left(1+\lambda\frac{\partial}{\partial t}+\beta\frac{\partial}{\partial t}\right)\frac{\partial u}{\partial t}=\left(1+\theta\frac{\partial}{\partial t}\right)\left[\frac{\partial^2 u}{\partial r^2}+\frac{1}{r}\frac{\partial u}{\partial r}\right]-M^2\left(1+\lambda\frac{\partial}{\partial t}+\beta\frac{\partial}{\partial t}\right)\left(U-Kt^n\right)$$
(14)

With the dimensionless initial and boundary conditions

$$u = \begin{cases} 0, & a \le r \le b & and & t \le 0 \\ 0, & at & r = 1 & t > 0. \\ 1, & at & r = r^* & t > 0 \end{cases}$$
(15)

where *M* is the Hartmann number and r^* is the radius ratio. The solution of Eq. (14) subject to the dimensionless initial and boundary conditions (15) can then be obtained by the Laplace transform technique. Now, define the Laplace Transform $\bar{u}(r,s) = \int_{0}^{\infty} u(r,t)e^{-st}dt$, (s > 0), where e^{-st} is kernel of the transform and *S* is the

transformed variable. Taking Eq. (15) taking into account, Eq. (14) becomes;

$$\left(s + \lambda s^{2} + \beta^{2}\right)\overline{U} = \left(1 + \theta s\right)\left[\frac{\partial^{2}\overline{u}}{\partial r^{2}} + \frac{1}{r}\frac{\partial\overline{u}}{\partial r}\right] - M^{2}\left(1 + \lambda s + \beta s\right)\left(\overline{U} - \frac{k}{s}\right).$$
(16)

Eq. (16) is reduced to a linear, non-homogeneous, ordinary differential equation of second order, having the form $\frac{d^2 \bar{u}}{dr^2} + \frac{1}{r} \frac{d \bar{u}}{dr} - \delta^2 \bar{u} = -\frac{M(1 + \lambda s + \beta s)}{s}.$ (17)

Together with boundary conditions

$$\bar{u} = \begin{cases} 0 & at \quad r=1\\ \frac{1}{s} & at \quad r=\lambda \end{cases}$$
(18)

Where $\delta^2 = \frac{\left(s + \lambda s^2 + \beta s^2\right)}{(1 + \delta s)} + \frac{M^2\left(1 + \lambda s + \beta s\right)}{(1 + \delta s)}.$

Eq. (17) represents the standard form of non-homogeneous Bessel equation and it solution is therefore given as;

$$\bar{u} = c_1 I_0(r\delta) + c_2 K_0(r\delta) + \frac{M^2 k (1 + \lambda s + \beta s)}{s\delta^2}.$$
(19)

where, I_0 , K_0 are the modified Bessel functions of first and second kind of order zero,

$$c_{1} = \frac{1}{s \left[I_{0}(\delta r^{*}) K_{0}(\delta) - I_{0}(\delta) K_{0}(\delta r^{*}) \right]} \left[K_{0}(\delta) + \frac{M^{2} k (1 + \lambda s + \beta s)}{\delta^{2}} \left\{ K_{0}(K_{0}r^{*} - K_{0}(\delta)) \right\} \right].$$

$$c_{2} = \frac{1}{s \left[I_{0}(\delta r^{*}) K_{0}(\delta) - I_{0}(\delta) K_{0}(\delta r^{*}) \right]} \left[\frac{M^{2} k (1 + \lambda s + \beta s)}{\delta^{2}} \left\{ I_{0}(\delta) - I_{0}(\delta r^{*}) \right\} - I_{0}(\delta) \right].$$

To obtain the inverse form of Equation (19) we use a numerical procedure used in an algorithm given by Tzou [18]. In this method, functions in the Laplace domain S can be inverted to the time domain t as follows;

$$u(r,t) = \frac{e^{\epsilon t}}{t} \left[\frac{1}{2} \bar{u}(r,\epsilon) + \operatorname{Re} \sum_{k}^{N} \bar{u}(r,\epsilon) + \frac{ik\pi}{t} (-1)^{k} \right].$$
⁽²⁰⁾

Where *Re* refers to the "real part of $i = \sqrt{-1}$ is the imaginary number, N is the number of terms used in the Riemann-sum approximation, and ϵ is the real part of the Bromwich contour that is used in inverting Laplace



transforms. Its accuracy depends on the value of ϵ and the truncation error dictated by N and the value of ϵ must be selected so that the Bromwich contour encloses all the branch points. For faster convergence, the quantity $\epsilon t = 4.7$ gives the most satisfactory results.

3.2 Skin Friction

The skin friction (or shear stress) $\tau_1(r,s)$ at the outer surface of the inner cylinder (r=1), and $\tau_{r^*}(r,s)$ at the inner surface of the outer cylinder $(r = r^*)$, in terms of the Laplace parameter s is computed by differentiating Eq. (19).

$$\frac{d\bar{u}}{dr}\Big|_{r=1} = \delta \Big[c_1 I_1(\delta) - c_2 K_1(\delta)\Big].$$
⁽²¹⁾

$$\frac{d\bar{u}}{dr}\Big|_{r=r^*} = \delta\Big[c_1 I_1(\delta r^*) - c_2 K_1(\delta r^*)\Big]$$
(22)

4. Results and Discussion

In order to get a physical insight into the problem, a MATLAB programme is written to compute and generate the graphs for the velocity, skin friction and mass flux in Figures 1 – 10 for various values of time (t), Hartmann number (M), relaxation time (λ), retardation time (θ) and Burgers' parameter (β) showing two cases when the magnetic field is fixed relative to the fluid (K = 0) and when the magnetic field is fixed relative to the moving outer cylinder (K = 1) represented by (a) and (b) respectively. The parametric values are arbitrarily chosen to study their effect on the flow domain. Figures 1 – 4 show the velocity profiles against r, depicting the effects of various non-dimensional parameters emerging in the flow model. Velocity is an increasing function of time and retardation time kr. It is decreasing function of relaxation times k; k1 and kinematic viscosity. Shear stress is an increasing function of time and retardation time kr. It is decreasing function of relaxation times k; k1 and dynamic viscosity.



Figure 1: Velocity profiles against r for different values of t and M = 5, $\lambda = 0.02$, $\theta = 0.02$, with K = 0 and K = 1 represented by (a) and (b).





Figure 2: Velocity profiles against r for different values of t and M = 0.5, $\lambda = 0.2$, $\theta = 0.2$ with K = 0 and K = 1 represented by (a) and (b).



Figure 3: Velocity profiles against r for different values of λ and M = 0.5, t = 0.2, $\theta = 0.2$ with K = 0 and K = 1, represented by (a) and (b).



Figure 4: Velocity profile against r for different values of θ and M = 0.5, t = 0.02, $\lambda = 0.2$ with K = 0 and K = 1, represented by (a) and (b).





Figure 5: Variation of skin frictions against t on the outer surface of the inner cylinder (r = 1) for different values of M and $\lambda = 0.2$, $\theta = 0.2$ with K = 0 and K = 1, represented by (a) and (b).



Figure 6: Variation of skin frictions against t on the inner surface of the outer cylinder (r = 2) for different values of M and $\lambda = 0.2$, $\theta = 0.2$ with K = 0 and K = 1, represented by (a) and (b).



Figure 7: Variation of skin frictions against λ on the outer surface of the inner cylinder (r = 1) for different values of θ and M = 0.5, t = 0.08 with K = 0 and K = 1, represented by (a) and (b).



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Figure 8: Variation of skin frictions against λ on the outer surface of the inner cylinder (r = 1) for different values of θ and M = 5.0, t = 0.08 with K = 0 and K = 1, represented by (a) and (b).



Figure 9: Variation of skin frictions against λ on the inner surface of the outer cylinder (r = 2) for different values of θ and M = 0.5, t = 0.08 with K = 0 and K = 1, represented by (a) and (b).



Figure 10: Variation of skin friction against λ on the inner surface of the outer cylinder (r = 2) for different values of θ and M = 5, t = 0.08 with K = 0 and K = 1, represented by (a) and (b).

5. Conclusions

In conclusion, semi analytical expressions for velocity and the associated skin friction (shear stress) for the MHD Couette flow of Burger's fluid in annuli are obtained. The expressions are given in Laplace transform domain with the aid of modified Bessel equations while the inverse of Laplace transform by using Riemann sum approximation as mentioned above. Impact of various physical parameters on the fluid velocity has been graphically presented. Significant features of the current analysis are as follows; (i) Increase in relaxation time (θ) increases the velocity. While increase in retardation time (λ) decreases the velocity. (ii) Increase in *M* decreases the velocity and the skin friction on the outer surface of the inner cylinder while the reverse is case on the inner surface of the outer cylinder.

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